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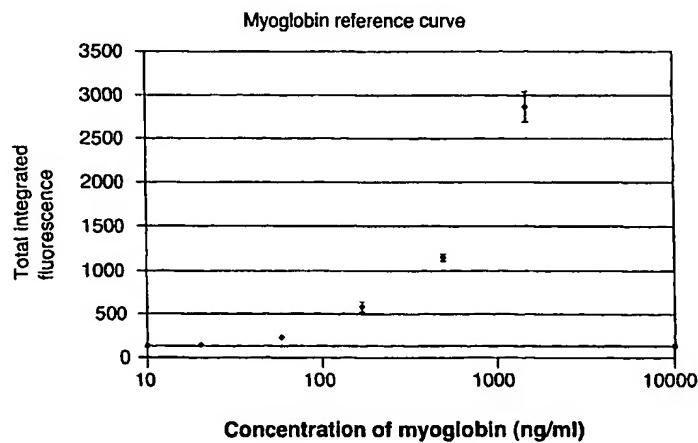
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(54) Title: CHARACTERIZATION OF REACTION VARIABLES



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(57) Abstract: A microscale method for the characterization of one or more reaction variables that influence the formation or dissociation of an affinity complex comprising a ligand and a binder, which have mutual affinity for each other. The method is characterized in comprising the steps of: (i) providing a microfluidic device comprising a microchannel structures that are under a common flow control, each microchannel structure comprising a reaction microactivity; (ii) performing essentially in parallel an experiment in each of two or more of the plurality of microchannel structures, the experiment in these two or more microchannel structures comprising either a) formation of an immobilized form of the complex and retaining under flow conditions said form within the reaction microactivity, or b) dissociating, preferably under flow condition, an immobilized form of the complex which has been included in the microfluidic device provided in step (i), at least one reaction variable varies or is uncharacterized for said two or more microchannel structures while the remaining reaction variables are kept essentially constant; (iii) measuring the presentation of the complex in said reaction microactivity in said two or more microchannel structures; and (iv) characterizing said one or more reaction variables based on the values for presentation obtained in step (iii).

CHARACTERIZATION OF REACTION VARIABLES.

TECHNICAL FIELD.

The present invention relates to a microscale method for the characterization of at least one reaction variable that influence the formation or dissociation of an affinity complex comprising a ligand and a binder. The ligand and the binder have affinity to each other and are affinity counterparts.

BACKGROUND TECHNOLOGY.

Microscale methods have previously been used for finding new combinations of ligands and binders for screening libraries of compounds for
(a) new drug candidates which are based on a receptor-ligand interaction, and
(b) new ligand candidates for affinity assays, affinity chromatography etc.

Microscale methods have also been suggested for optimizing the conditions for formation or dissociation of a particular affinity complex or when selecting affinity counterparts for other reasons.

Microscale methods have also been used for determining the amount of a particular compound (analyte) in a sample.

Methods have been used that are based on affinity capture of a binder or an analyte by an affinity counterpart that is immobilized or immobilizable to a solid phase.

Typically the formation of the complex on a solid phase has been performed under non-flow-conditions. See for instance Eteshola et al, Sensors and Actuators B 72 (2001) 129-133; Sato et al, Anal. Chem. 72 (2000) 1144-1147; and WO 9721090 (Gamera, Mian et al).

Non-flow conditions will simplify the methods but information that only can be obtained from experiments performed under flow conditions will be missed. For small molecules non-flow conditions may be acceptable because their diffusion

rates are often relatively high and orientation of their binding sites for binding is uncomplicated. This is normally not applicable to larger molecules. Without controlling the liquid flow accurate information will be difficult to obtain for large molecules.

Recently a MALDI MS integrated microfluidic affinity system based on affinity binding to a reverse phase matrix has been presented. In this system a protein digest was adsorbed to a reverse phase matrix and subsequently desorbed and transported to an outlet port that functioned as a MALDI MS target. (*Integrated sample preparation and MALDI MS on a microfluidic compact disc* (CD with improved sensitivity) (Magnus Gustavsson et al) ASMS 2001. The demand on the reproducibility in the binding, the control of the liquid flow rate, and the residence time was low.

WO 0138865 (Univ. of Alberta, Harrison et al) describes a solid phase extraction method in a singular microchannel structure utilizing flow conditions and affinity binding. In another example the publication shows saturation of solid phase bound anti-theophylline antibodies with theophylline.

DEFINITIONS.

Reaction variables are mainly of two kinds: 1) variables related to affinity reactants with the subgroups a) amounts including presence and/or absence, and b) properties of affinity reactants including affinity, and 2) reaction conditions.

Group 1a comprises amounts in mass units, molar units, relative amounts, concentrations, activity/mass unit, activity/volume unit, relative activities etc. Activity refers to (i) biological activity, (ii) binding activity for an affinity counterpart etc. Biological activity includes enzyme activity binding activity towards a native or synthetic affinity counterpart, cell activity etc.

Group 1b comprises properties of an affinity reactant (a ligand and/or a binder).

Typically this group comprises properties of inhibitors and promoters for the formation or dissociation of an affinity complex, enzymes, substrates, cofactors, cosubstrates, coenzymes, receptors, hormones, antibodies and antigen/hapten-binding fragments thereof, antigens/haptens etc. Synthetic and recombinant forms are included.

If a variable of group 1b varies or are different between samples, microchannel structures, reaction microcavities, aliquots of liquid etc this primarily means that different molecular entities are present in respective unit.

The properties related to group 1b comprises affinity which includes affinity constants (and the corresponding constant for the dissociation), rates for formation and dissociation, knowledge about counterpart(s) towards which a binder has/have affinity and vice versa (specificity, selectivity etc) etc. Affinity also comprises relative affinity of different complexes, for instance a common ligand versus a range of binders and vice versa, a common complex versus changes in reaction conditions etc.

Reaction conditions in this context means reaction variables that are not related to a property of an affinity reactant. Reaction conditions comprise pH, temperature, ionic strength (including type of salts), hydrogen bond breaking agents (denaturing agents, amount and kind)), detergents (amount and kind), liquid flow, immobilization techniques, solid phases etc.

Affinity reactants (ligands and binders) that are to be characterized with respect to group 1 variables are called "analytes". The term "Analyte" also includes analyte-derived entities that originate from an original analyte in an original sample that has been processed to the sample used in the microfluidic device for step (ii). This preprocessing may take place outside the microfluidic device and/or in separate substructures within the microfluidic device. The amount of an analyte-derived entity in a processed sample is a function of the occurrence of

the original analyte in the original sample.

The term "analogues" is used for two or more binders or ligands that are capable of inhibiting or competing with each other for affinity binding to a common affinity counterpart. In the same manner "analogue" is also used for an analyte.

A microfluidic device comprises at least one microchannel structure through which liquid flow is used for the transport of reactants

The terms "microformat", "microchannel" etc contemplate that a microchannel structure comprises one or more cavities and/or channels that have a depth and/or a width that is $\leq 10^3 \mu\text{m}$, preferably $\leq 10^2 \mu\text{m}$. The volumes of microcavities/microchambers are typically $\leq 1000 \text{ nL}$ (= nL-range), such as $\leq 500 \text{ nL}$ or $\leq 100 \text{ nL}$ or $\leq 50 \text{ nL}$, but may also be larger, i.e. in the interval 1-1000 μl , such as 1-100 μl or 1-10 μl .

The term "microfluidic method" means that (a) the method is performed in a microfluidic device, and (b) the liquid volumes are in the microformat.

A "library" is a set of two, three, four or more compounds or substances, for instance ≥ 10 , such as ≥ 100 or ≥ 1000 or ≥ 10000 . Typical examples are recombinant, synthetic or native sets of nucleotides, oligonucleotides, polynucleotides, amino acids, oligopeptides, polypeptides, proteins, lipids, other organic and inorganic compounds, carbohydrates, bacteria, phages, polymers, biopolymers etc. Each individual library may contain members of different classes, for instance polypeptides and polynucleotides, carbohydrates and proteins etc. A library may also include sets that are derived from nature, e.g. sets of native proteins in which the individual proteins relate to each other due to post-translational modifications, isoproteins such as isoenzymes etc. Examples of post-translational modifications that can result in a library are phosphorylation,

activating cleavage, glycosylation, ubiquitination, etc.

The term "library" also includes sets of other reaction variables, such as different pH values, different immobilization groups, different ionic strengths, different concentrations, different salts, different solid phases, different spacers etc.

The "library" also includes a collection of samples (aliquots of liquid) differing with respect to at least one reaction variables.

OBJECTS OF THE INVENTION.

A first object is to provide an improved microscale method for quantifying the amount of an analyte in a plurality of samples by using assay methods that are based on specific affinity binding and capture to a solid phase

A second objective is to provide a fluidic function that when incorporated into the microchannel structures of a microfluidic device will standardize the flow rate in the individual microchannel structures in a microfluidic device, i.e. to control the flow rate such that the inter-channel variation is reduced to an acceptable level.

A third objective of the present invention is to provide a robust microfluidic system and method that can be used for parallel screening of reaction variables in order to find new and optimal binder-ligand combinations and/or to grade affinity for a range of affinity complexes, ligands and binders, and/or to optimize processes involving formation or dissociation of immobilized affinity complexes under flow conditions.

These objects primarily concern methods which utilize interactions involving at least one affinity reactant which is relatively large and/or comprises one or more functional groups comprising a heteroatom selected amongst nitrogen, oxygen, sulphur and phosphorous. Relatively large in this context means that the affinity reactant simultaneously can bind two affinity counterparts and/or has a molecular

weight \geq 1000 dalton, such as \geq 2000 or \geq 10000 dalton. Typically one of the affinity reactants is polymeric, such as a biopolymer comprising carbohydrate structure and/or peptide structure and/or nucleotide structure and/or lipid structure. Molecules that are not large are considered to be small.

FIGURES:

Figures 1a and 1b illustrate a variant of a preferred microchannel structure that has a narrow microconduit that create a significant pressure drop. This variant has been used for the model study presented in the experimental part. **Figures 1a and 1b** are identical except that **figure 1a** gives the dimensions and **figure 1b** hydrophobic surface breaks and their dimensions.

Figure 2 illustrates a set of microchannel structures of the same kind as used in the experimental part. The structures are linked together by a common distribution channel and a common waste channel.

Figure 3 illustrates the key part of a substructure that comprise a reaction microcavity and means for creating a pressure drop.

Figure 4 represents the results obtained in the experimental part. The structures shown in **figures 1-2** are intended to be placed on a circular disc around its axis of symmetry (spinning axis). The arrow shows the direction towards the center of the disc. Note also the arc-like configuration.

SUMMARY OF THE INVENTION

The present inventors have recognized that the method defined under "Technical Field" above can be improved by

- (a) utilizing a microfluidic device comprising two or more microchannel structures in which the flow is under a common flow control, and
- (b) performing formation of the affinity complex under flow conditions in at least two of the microchannel structures and retaining an immobilized form of the formed affinity complex under flow conditions in a reaction microcavity in each

of the microchannel structures used.

In a similar manner the principle of common flow control and flow conditions are applied to the dissociation of an affinity complex retained in the reaction microcavity for the characterization of reaction variables influencing the dissociation reaction.

The inventors have also recognized a number of additional features that can reduce the effects of variations in flow between different microchannel structures within the same device (inter-channel variation):

- (a) A means for flow restriction downstream the reaction microcavity in each microchannel structure for creating a significant pressure drop.
- (b) A porous matrix placed in a desired part, for instance the reaction microcavity or immediately downstream the reaction microcavity, of each microchannel structure for creating a significant pressure drop.
- (c) A packed bed of monosized particles instead of polysized particles in the reaction microcavity.
- (d) a pulse giving increased flow will assist in over-coming inter-channel variations in flow resistance, in particular when initiating flow and/or when the liquid is to pass through branchings and curvatures.
- (e) Anti-wicking means in inner edges downstream and in close proximity to the outlet end of the outlet microconduit which leads waste liquids from a reaction microcavity.
- (f) Excess of solid phase affinity reactant (e.g. binder (immobilized reactant)) in the reaction microcavity.
- (g) Selecting flow rates that accomplish residence times ≥ 0.010 seconds for the formation of complex in the reaction microcavity.

Significant pressure drop is relative to inter-channel variations in flow resistance.

DETAILED DESCRIPTION OF THE INVENTION.

The invention is a microscale method for characterizing at least one reaction variable. The method is generally defined in the first paragraph. The characterizing feature comprises four steps:

Step (i): Providing a microfluidic device comprising a plurality of microchannel structures that are under common flow control. Each of the structures comprises a reaction microcavity for retaining an affinity complex.

Step (ii): Performing essentially in parallel an experiment in each of two or more of the plurality of microchannel structures. Each experiment comprises:
(a) forming an immobilized form of the complex and retaining under flow conditions this form within the reaction microcavity, or
(b) dissociating an immobilized form of the complex within the reaction microcavity.

The reaction variables referred to are different and/or are uncharacterized for two or more of the experiments. Other reaction variables are kept essentially constant. Dissociating is typically performed under flow conditions. The immobilized form in (b) is introduced prior to step (ii). The formation of the retained complex is a function of the introduction of the ligand and the binder.

Step (iii): Measuring the presentation of the complex in the reaction microcavity in each of said two or more microchannel structures.

Step (iv): Characterizing said at least one reaction variable based on the values for presentation which is measured in step (iii).

The experiments are initiated by introducing the appropriate liquid aliquots into inlet ports of the device and applying the appropriate driving force for liquid flow.

In the same microfluidic device there may also be run other similar or dissimilar experiments in parallel with those defined above.

The term "essentially constant" in this context means that the other variables are kept within ranges where the outcome of the experiments will be essentially the

same.

In the preferred variants, the reaction microcavities to be used in the method and provided in step (i) comprise an affinity reactant (affinity binder) that in step (ii) will be incorporated into the immobilized complex.

COMMON FLOW CONTROL AND LIQUID FLOW CONDITIONS FOR STEP (STEPS (i) AND (ii)).

The term "common flow control" means that when a driving force for a liquid flow is applied in one part of a microchannel structure (structure 1), there will also be applied a driving force for liquid flow in the corresponding part of each of the other microchannel structures of the device. The driving force in the individual channels derives from the same source, e.g. spinning the device if centrifugal force is the driving force. Moreover, an increase or a decrease in driving force in one microchannel structure is paralleled with an increase or a decrease in the other microchannel structures. The size of the force (and the liquid flow rate) may differ between different microchannel structures for which common flow control is applied. In centrifugal based systems, for instance, the designs of the microchannel structures may differ and/or the microchannel structures may be placed at different radial distances.

Common flow control primarily refers to the flow through the reaction microcavity (solid phase) when the immobilized complex is formed and retained. Flow control may be less critical in other parts of the structures and/or for other steps of the method.

The liquid flow may be driven by distinct means that either is present in or external to the device. Thus, liquid flow may be created by electroosmosis, micropumps, expanding gas etc. Another alternative is to use forces such as capillary force and inertia force including gravitational force and centrifugal force to drive the liquid, i.e. forces which do not require any means on the microfluidic device.

The appropriate flow rate through the reaction microcavity (step (ii)) depends on a number of factors, such as the affinity pair used for forming the immobilized complex, the volume of the reaction microcavity, the solid phase in the microcavity etc. Typically the flow rate should give a residence time of ≥ 0.010 seconds such as ≥ 0.050 sec or ≥ 0.1 sec with an upper limit that typically is below 2 hours such as below 1 hour. Illustrative flow rates are within 0.01-100 nl/sec, typically 0.1 - 10 nl/sec. Residence time refers to the time it takes for a liquid aliquot to pass through the reaction microcavity (i.e. through the solid phase).

An acceptable flow control depends on a particular application including concentrations of reactants, their diffusion properties and reaction rates, etc. Sufficient flow control in most cases means that the intra-channel variation for residence time is within the mean residence time $\pm 90\%$, such as $\pm 75\%$ or $\pm 50\%$ or $\pm 25\%$.

According to a preferred variant of the invention, common flow control is accomplished by spinning a microfluidic device in which the microchannel structures are oriented from an inward position to an outward position in relation to an axis of symmetry of a substrate and utilizing the centrifugal force for driving the liquid. Common flow control also include that centrifugal force is used to create a sufficient local hydrostatic pressure within a structure to drive a liquid aliquot through an outward (downward) and/or an inward (upward) bent of a microchannel structure. See for instance WO 0146465 (Gyros AB).

Typical spinning speeds are within the interval 50-25000 rpm, such as 50-15000 rpm. The spinning speed within a given protocol may vary, for instance comprise sequences with individual ramps of acceleration, deceleration, and constant spinning. It may be beneficial to include a pulse of increased spinning at certain

positions. See above.

MICROFLUIDIC DEVICE (STEP (i)).

The present invention is primarily intended for geometric arrangements in which the microchannel structures are present in a substrate (microfluidic device) that has an axis of symmetry. Each microchannel structure is then oriented in an outward direction relative to the axis of symmetry, i.e.

- (a) the reaction microcavity is part of a substructure which also comprises a structural unit delivering liquid to the reaction microcavity, and
- (b) the latter unit is at a shorter radial distance than the reaction microcavity and communicates with an inlet port.

An inlet port is typically located at a shorter radial distance than the reaction microcavity. Downstream the reaction microcavity there may be an outlet port, typically located at a larger radial distance than the reaction microcavity. By utilizing capillary force and/or other non-centrifugal forces for the introduction of a liquid into a microchannel structure, inlet ports may be located at in principle any radial distance, e.g. more remote from the axis of symmetry than an outlet port and/or the reaction microcavity.

The microchannel structures may or may not be oriented in a plane perpendicular to the axis of symmetry.

In centrifugal based systems a "higher" or an "upper" level/position will be at a shorter radial distance (inner position) compared to a "lower" level/position (outer position). Similarly, the terms "up", "upward", "inwards", and "down", "downwards", "outwards" etc will mean towards and from, respectively, the spinning axis. This applies if not otherwise is specified. With respect to other arrangement substrates and conventional driving forces, i.e. gravity force, externally applied pressure, electro-osmotically driven flows etc, these terms have their conventional meaning.

Axes of symmetry are n-numbered (C_n) where n is an integer between 2 and ∞ , preferably 6, 7, 8 and larger, for instance ∞ . In preferred cases the substrate (microfluidic device) as such may have a circular, cylindrical, spherical or conical symmetry (C_∞).

The preferred devices are typically disc-shaped with sizes and forms similar to the conventional CD-format, e.g. in the interval from 10% up to 300 % of the conventional CD-radii.

Suitable microfluidic devices may be manufactured from a planar substrate surface comprising a plurality of uncovered microchannel structures that in a subsequent step are covered by another planar substrate (lid). See WO 9116966 (Pharmacia Biotech AB) and WO 0154810 (Gyros AB). At least one of the substrates may be transparent, e.g. the second substrate (lid). Both substrates are preferably fabricated from plastic material, e.g. plastic polymeric material.

Different applications require different surface characteristics. This means that in the case aqueous liquids are to be transported within the microchannel structures hydrophilization may be required. See for instance WO 0056808 (Gyros AB) and WO 0147637 (Gyros AB). For aqueous liquids an essential part of the inner surfaces should have water contact angles $\leq 90^\circ$, such as $\leq 40^\circ$ or $\leq 30^\circ$ or $\leq 20^\circ$ at the temperature of use. At least two or three of the inner walls enclosing the channels should comply with this range. Surfaces in passive valves, anti-wicking means etc are excluded from these general rules.

Non-wettable surface breaks may be introduced at predetermined positions in the inner walls of the microchannel structures before covering the uncovered microchannel structures (WO 9958245, Amersham Pharmacia Biotech AB) and WO 0185602, Åmic AB & Gyros AB). For aqueous liquids this means hydrophobic surface breaks. Surface breaks may be used for controlling the

liquid flow within the structures, e.g. anti-wicking, passive valves, directing liquids etc. See below. In figure 1a, surface breaks are cross-hatched and openings (inlets, outlets, vents) in the covering substrate (lid) are represented by hatched circles.

Figures 1a-b and 2 illustrate a microchannel structure (101) that can be used in the present invention. The structure comprises a reaction microcavity (104) connected to one or more inlet microconduits (102 and 103) and an outlet microconduit (105) with an outlet end (106). When the structure is used the immobilized complex becomes retained in the reaction microcavity (104). Alternatively the reaction microcavity contains the affinity complex from the beginning and the method means dissociation of the complex.

If there are two or more inlet microconduits (102 and 103) they typically merge before reaching the reaction microcavity (104). In the case the reaction microcavity contains a solid phase in form of particles the trespass into the outlet microconduit (105) typically is a sharp drop in the cross-sectional area that prevents the particles from passing into the outlet microconduit.

For centrifugal based systems, two inlet microconduits (102 and 103) typically form at downward bent (107) with shanks corresponding to the inlet microconduits (102 and 103). The outlet microconduit (105) is connected to the lower part of the bent via the reaction microcavity (104).

An inlet microconduit (102,103) may be connected to an inlet port (108,208 and 209 and 210) via a functional unit. This unit may be a volume-defining unit (111) that comprises a metering microcavity (112) connected to one of the inlet microconduits (102), an overflow channel (113) that starts in a narrow conduit part between the metering cavity (112) and the inlet unit (114) and ends in a waste function, for instance comprising a common waste reservoir/channel (115,215). The waste function may have one or more outlet ports (116,216). The

volume-defining unit (111) comprises valve functions (117,118) that are associated with the overflow channel (113) and with the outlet end of the metering microcavity (112). For centrifugal based systems these valve functions are typically passive and preferably based on local changes in surface characteristics. The valve function (118) is at a larger radial distance than the valve function (117). This means that the positions of these valves are selected to support that liquid in the overflow channel (113) is passed into the waste function at a lower spinning speed than liquid in the metering microcavity (112) is passed into the inlet microconduit (102). A volume-defining unit of this kind (111) is primarily intended for liquid aliquots that are to be introduced with high accuracy with respect to volume. This means liquid aliquots that contain

- (a) an analyte and/or
- (b) a reaction variables of group 2 that varies between microchannel structures and/or
- (c) any other reagent that has to be delivered with a high accuracy.

Aliquots of type (a) and (b) will be called aliquot 1.

An alternative functional unit connected to one of the inlet microconduits (102,103) is a unit for distributing liquid aliquots to separate microchannel structures. The unit may be in the form of a distribution channel (119,219) that is common for several microchannel structures (101,201). For centrifugal based system the channel may have alternating upper and lower parts (120,220 and 121,221, respectively) with an inlet vent (122,222) to ambient atmosphere in each upper part (120) and liquid communication in each lower part (121) via a valve function (123) to one of the inlet conduits (103,203) of each microchannel structure (101,201). The vents (122,222) communicate with ambient atmosphere via a common venting channel (124,224). The distribution channel may have one or more inlet ports (209,210) and one or more outlet ports (125,225) (only one shown).

As shown in the figures the outlet end (106) may mouth into a waste conduit

chamber (126) (belonging to the microchannel structure). This chamber in turn may mouth into a common waste conduit or a common waste reservoir (115). Although not preferred, the outlet conduit (105) may in an alternative variant mouth directly into a common waste chamber or into ambient atmosphere. For centrifugal based systems utilizing passive valves, the outlet end (106) of the outlet microconduit (105) typically is at the same or a higher level than the reaction micocavity (preferably its top part) (104). According to one inventive aspect of the invention the outlet microconduit (105) possibly in combination with a solid phase in the reaction microcavity (104) are able to produce a pressure drop against a liquid flow passing through the microchannel structure, which is significantly larger than the resistance to flow upstream the reaction microcavity (104). The pressure drop in a microconduit is proportional to its length and inversely proportional to its hydrodynamic cross-sectional area.

In the invention the pressure drop across the outlet microconduit (105) between the reaction microcavity (104) and the waste chamber (126) should be large enough to level out intra-channel differences (variations) in flow resistances that primarily depend on (a) inner surface characteristics upstream the reaction microcavity and (b) the solid phase used (for instance the packing geometry may differ).

The principles outlined have lead to the design of the microchannel structures used in the experimental part (figures 1-2):

- (a) Reaction microcavities (104) with a depth of 100 µm and width of 250 µm,
- (b) Outlet microconduits (105) with a depth of 10 µm, a width of 20 µm and a length of 4.56 mm.

Other parts of the microchannel structures had a depth of 100 µm.

There may be vents to ambient atmosphere at appropriate positions to

- (a) level out over-pressure that may be created in "dead-ends" when liquid is

introduced into a microchannel structure, or
(b) interrupt flow at certain positions.

In the variant illustrated in the figures 1-2, the second kind is present in inlet port (108,208). Venting functions (122,222 and 127,227) that break a liquid flow are also present in the common distribution channel and in the waste chamber (119,219 and 126,226, respectively).

The inlet ports (108,208 and 209 and 210) preferably are connected to a microcavity (128), which typically is narrowing inwards the microchannel structure and has longitudinal projections (ridges) (129) in the flow direction. These ridges will facilitate quick transport of a dispensed liquid aliquot into the interior of an inlet unit. The inlet ports also may have a non-wettable area (typically hydrophobised) (130, cross-hatched) that will direct a dispensed liquid into the inlet unit (114).

In order to avoid undesired loss and transport of liquid via wicking, the microchannel structures may be equipped with anti-wicking means at selected positions in form of changes in surface characteristics. The changes are typically local and may be related to geometric surface characteristics (131) and/or chemical surface characteristics (132,133)(cross-hatched area). See WO 9958245, Amersham Pharmacia Biotech AB and U.S. S.N. 60/315,471 and the corresponding International Patent Application. For aqueous liquids this means that the change is from hydrophilic to hydrophobic. There is also an anti-wicking function (134,135,123,117) (cross-hatched) present at the inlet vents (127,122) and in the passive valves (123,117).

Valves are preferably passive, i.e. passage of a liquid will depend on the applied driving force and the physicochemical match between a liquid and the inner surface at the valve position. No movable mechanical parts are needed.

Examples are capillary valves that are based purely on a change in geometric surface characteristics (WO 9615576 (David Sarnoff Res. Inst.) and WO

9807019 (Gamera). Preferred passive valves are based on a change in chemical surface characteristics, i.e. non-wettable surface breaks. For aqueous liquids this means hydrophobic surface breaks (WO 9958245, Amersham Pharmacia Biotech AB). Valves may also be based on a combination of changes in both chemical and geometric surface characteristics. The changes are typical local. See also U.S. S.N. 60/315,471 and the corresponding International Patent Application. Other kinds of valves may also be used.

More details about inlet units, distribution units, volume-defining units, waste conduits, anti-wicking means and valves, in particular for centrifugal based systems, are given in U.S. S.N. 60/315,417 and the corresponding International Patent Application.

Reaction microcavity and solid phase.

The geometry of reaction microcavity (104) is preferably a straight microchannel that may be continuously widening and/or narrowing. At least a part of the wall of the reaction microcavity is transparent with respect to the principle used for measuring the presentation of the complex.

The reaction microcavity preferably comprises a catching affinity reactant immobilized to a solid phase, which is kept within the reaction microcavity.

The solid phase is derivatized with a reactant (capturing reactant) that can be incorporated by affinity into the affinity complex that is formed in immobilized form in step (ii). The capturing reactant may be an immobilized form of the ligand or the binder.

The solid phase may be the surface of the inner wall of the microcavity (104), the inner surface of a porous monolith that wholly or partly will occupy the interior of the reaction microcavity or a population of porous or non-porous particles that are packed to a bed. In the case the solid phase comprises particles there should be

retaining means associated with the downstream end of the reaction microcavity. This means is preferably in the form of a constriction, e.g. in the form of a barrier, that prevents the particles from leaving the microcavity. The particle diameter/size should at least be of the same size as or larger than the smallest dimension of the opening in the constricted part. Another kind of retaining means is magnetic particles combined with an externally applied magnetic field.

A porous monolith may be fabricated in one piece of material or may comprise particles that are attached to each other.

By the term "porous particles" is meant that the particles can be penetrated by soluble reactants that are to be incorporated into the affinity complex. This typically means Kav values within the interval of 0.4 -0.95 for these reactants. Non-porous particles have a Kav-value below 0.4 with respect to the same reactants. Porous monoliths have pores that are large enough to permit mass transport of the reactants through the matrix by the liquid flow applied.

The particles may be spherical or non-spherical. With respect to non-spherical particles, diameters and sizes refer to the "hydrodynamic" diameters.

The particles are preferably monodisperse (monosized) by which is meant that the population of particles placed in a reaction microcavity has a size distribution with more than 95 % of the particles within the range of the mean particle size \pm 5 %. Population of particles that are outside this range are polydisperse (polysized).

The solid phase may or may not be transparent for the principle used for measuring the complex.

The material in the solid phase, e.g. the particles, is typically polymeric, for

instance a synthetic polymer or a biopolymer. The term biopolymer includes semi-synthetic polymers comprising a polymer chain derived from a native biopolymer. The particles and other forms of solid phases are typically hydrophilic in the case the liquid flow is aqueous. In this context hydrophilic encompasses that a porous solid phase, e.g. a packed bead, will be penetrated by water. The term also indicates that the surfaces of the particles shall expose a plurality of polar functional groups in which there is a heteroatom selected amongst oxygen, sulphur, and nitrogen. Appropriate functional groups can be selected amongst hydroxy groups, straight ethylene oxide groups ($[-\text{CH}_2\text{CH}_2\text{O}-]_n$, n an integer > 0), amino groups, carboxy groups, sulphone groups etc, with preference for those groups that are neutral independent of pH. A hydrophobic particle may be hydrophilized, for instance by introducing hydrophilic groups. See for instance the experimental part. The coating technique is similar to the technique presented in WO 9800709 (Pharmacia Biotech AB, Arvidsson & Ekström).

The techniques for immobilization may be selected amongst those that are commonly known in the field, for instance the bonding to the solid phase may be solely via covalent bonds, affinity bonds (for instance biospecific affinity bonds), physical adsorption (mainly hydrophobic interaction) etc. Examples of biospecific affinity bonds that can be used are bonds between streptavidin and a biotinylated affinity reactant, high affinity antibody and a haptensylated affinity reactant etc.

Other functional units in the microchannel structures.

A microchannel structure may also comprise separate or combined units that enables:

- (1) separation of particulate matter from a liquid aliquot introduced via an inlet port,
- (2) mixing, e.g. for the formation of an affinity complex upstream the reaction microcavity, and
- (3) detection of (a) a reactant that has passed through the reaction microcavity, or (b) a component released from the complex formed in the reaction

microcavity.

Except for unit 3, these functional units if present may be located upstream the reaction microcavity.

A unit for separation of particulate matter is typically positioned upstream a volume metering unit or the two units are combined in a common unit.

Preferred separation units, volume metering units and mixing units are given in U.S. S.N. 60/315,417 and the corresponding International Application.

Additional units may also be present.

The presence of units 1-2 means that the protocol used for step (ii) may include at least one substep selected from

- (ii.a) a separation step, and
- (ii.b) a mixing step that may include formation of the affinity complex that is retained in immobilized form in the reaction microcavity.

The separation step may be carried out simultaneously with a volume-metering step if each of the microchannel structures used can utilize a combined separation/volume metering unit. Otherwise the separation step is typically upstream a volume-metering step, in particular if the separation step is used to clean a sample. A mixing step, if present, is typically downstream a volume metering step.

A separate detection microcavity may enable measuring of:

- an analytically detectable entity that is released from the complex retained in step (ii),
- an enzyme product in the case the complex has enzyme activity and a substrate has been passed through the reaction microcavity subsequent to

step (ii),

- a compound passing through the reaction microcavity as a functional control,
- a second analyte by retaining an immobilized form of a complex that is different from the complex retained in step (ii),
- a standard compound (calibrator) that is passing through the reaction microcavity without interfering with steps (ii) and (iii).

The first two alternatives may also be part of step (iii).

PROTOCOLS COMPRISING FORMATION OR DISSOCIATION OF AN IMMOBILIZED COMPLEX IN THE REACTION MICROCAVITY (STEP (ii)).

A. Determination of an uncharacterized amount of an analyte.

These protocols are selected amongst biospecific affinity assays that are used for the determination of an analyte in a sample. The principles are well known in the field. The protocols encompass that one or more affinity counterparts to the analyte are used for the formation of an affinity complex which is then measured and related to the amount of the analyte in a sample. The assay conditions are selected such that the amount of the complex becomes a function of the amount of analyte in the sample.

In the variants used in the invention, the complex to be measured corresponds to the immobilized complex retained in a reaction microcavity in step (ii). Depending on the protocol used this complex may or may not comprise the original analyte of the original sample introduced into the microfluidic device. Reaction variables other than the amount of analyte are in principle kept essentially constant for experiments run in different microchannel structures.

Step (ii) may comprise introduction of one or more additional reactants that will become incorporated into the retained complex in order to facilitate its measurement in step (iii). Similarly step (iii) may comprise introduction of one or

more additional reactants that might be needed for the measurement of the complex formed in step (ii).

The affinity reactant that defines the link between the solid phase and the immobilized complex to be measured in step (iii) may be introduced by the manufacturer and therefore provided in step (i). Other reactants, including the analyte, are introduced in subsequent steps. This may be done in sequence, in parallel, and/or as mixtures. One or more additional inlet ports may be used. If needed, mixing of affinity reactants and liquids may take place within separate mixing units that are located upstream the reaction microcavity.

According to the invention, amounts can be determined during both diffusion-limiting and non-diffusion-limiting conditions if proper care has been taken. The flow rate may in principle be used to secure that the conditions contemplated are at hand, the general guide-line being that a decrease in flow rate (increase in residence time) will favor non-diffusion limiting conditions and vice versa for diffusion-limiting conditions. These rules primarily apply to large molecules.

Competitive/inhibition protocols.

In these protocols the analyte and an analyte analogue are competing with each other for binding to a limiting amount of an affinity counterpart to the analyte. This counterpart may be

- (a) immobilized or immobilizable if the analyte analogue is soluble and analytically detectable, and
- (b) analytically detectable if the analyte analogue is immobilized or immobilizable.

At the filing date variant (b) is of great interest for the invention. This variant includes that the analyte and its affinity counterpart are preincubated before reaching the reaction microcavity, for instance outside the microfluidic device or in a separate mixing microcavity upstream the reaction microcavity. The mixture

is transported through the reaction microcavity where the free (=uncomplexed) affinity counterpart forms an affinity complex with an immobilized analyte analogue. This complex is subsequently measured in step (iii).

Competitive variants also include displacement assays in which an immobilized or immobilizable affinity complex comprising two affinity counterparts is incubated with a sample containing an analyte. Provided that one of the affinity counterparts is an analytically detectable analyte analogue, the analyte will displace the analyte analogue in the complex, which also means that the signal from the complex will change.

A preferred displacement assay is to provide this kind of complex in immobilized form in the reaction microcavity in step (i). In step (ii) the analyte will displace the analyte analogue of the immobilized complex. In step (iii) the amount of complex containing the analyte is measured directly in the reaction microcavity or indirectly from released analytically detectable analyte analogue in a separate detection microcavity downstream the reaction microcavity.

Competitive variants are particularly adapted for analytes that have difficulties in binding two or more affinity counterparts simultaneously, i.e. relatively small molecules.

Non-competitive protocols

These protocols typically utilize non-limiting amounts of one or more affinity counterparts to the analyte.

The most important non-competitive protocols are sandwich protocols which comprise formation of immobilized or immobilizable complexes in which an analyte is sandwiched between two affinity counterparts. One of the counterparts is analytically detectable and the other immobilized or immobilizable and possibly also analytically detectable. The sandwich complex is measured in step (iii).

Another non-competitive variant utilizes only one affinity counterpart to the analyte in immobilized or immobilizable form. In this case complex formation leads to an immobilized complex, or a soluble complex that subsequently is immobilized. The immobilized complex as such may be measured in step (iii). In one variant the affinity counterpart which is immobilized or immobilizable has been labeled with an analytically detectable group that changes its signal when the analyte binds to the affinity counterpart.

Non-competitive protocols have their greatest potential for molecules that simultaneously can bind two or more affinity counterparts, i.e. large molecules.

Analytically detectable reactants.

By the term "analytically detectable" is contemplated that an affinity reactant can be analytically discriminated from other affinity reactants participating in the formation of the complex to be measured in step (iii). Detectability may derive from an inherent property of the reactant, for instance an inherent biological function such as the enzyme activity of an enzyme or Fc-receptor binding activity of various Ig-classes and subclasses, or a separately introduced functionality, e.g. labeling with an analytically detectable tag or label, such as biotin (= affinity label), enzyme, chromogen, fluorogen, fluorophor, chemiluminescent group, radioactive group etc. Detectability also includes that the formed complex is detectable by itself, for instance by changing the optic properties of a solution etc.

A detectable label may be combined with a second label selected such that the labels together give the appropriate signal when the complex is formed or dissociated. This variant may be illustrated with scintillation proximity assays (SPA) in which a soluble affinity reactant, which is labeled with tritium, is used together with a solid phase comprising a scintillation substance. When the tritium-label becomes incorporated in a complex bound to this kind of solid phase a signal will appear. The principle with interacting labels may also be illustrated with pairs of fluorophores that may be identical or different and with fluorescence-

quencher pairs.

An illustrative variant of running several samples in parallel

Step (i): The microfluidic device is as discussed above and comprises k microchannel structures (k is an integer 2 or larger), each of which comprises an immobilized affinity counterpart to an analyte or a combination of such counterparts. The affinity counterparts may or may not differ between the microchannel structures. The affinity counterparts are preferably located to the reaction microcavities in which the affinity complex is to be retained.

Step (ii): A liquid aliquot (aliquot 1) that contains an unknown amount of analyte is introduced into n of the k microchannel structures which contain the affinity counterparts, i.e. aliquot 1¹ into microchannel structure 1, aliquot 1² into microchannel structure 2 . . . and aliquot 1ⁿ into microchannel structure n, where n is an integer equal or smaller than k. Possibly there is also introduced an aliquot containing a known amount of analyte into at least m of the remaining microchannel structures, if any, i.e. aliquot 1ⁿ⁺¹ into microchannel structure n+1, aliquot 1ⁿ⁺² into microchannel structure n+2 . . . and aliquot 1^{n+m} into microchannel structure n+m, where m is an integer such that n+m is equal or smaller than k . The aliquots with their possible content of analyte are then transported through the microchannel structures such that immobilized complexes will be retained under flow conditions in the reaction microcavity of each microchannel structure. For aliquots that contain no analyte there will be no formation of complex.

Steps (iii) and (iv): The amount of the immobilized complex in each reaction microcavity is measured and related to the amount of analyte in the corresponding starting aliquot/sample.

With respect to reactants and their addition, similar protocols as those discussed above may be used for variants B-F below. In these variants the demand on using limiting and unlimiting amounts may be less important. For alternatives B-

D, the concentration and/or relative amounts of the affinity reactants used are typically essentially constant for several of the experiments run in parallel according to the invention. Variants B-F are primarily run under non-diffusion-limiting conditions.

B. Selection of binders (analytes) from a library of potential binder candidates.

Two preferred variants are:

- A) Different binder candidates and/or combinations of binder candidates from a library are used in immobilized form in two or more of the microchannel structures of the microfluidic device provided in step (i). A soluble form of a known common ligand is used to form the immobilized complex in step (ii).
- B) The same known immobilized ligand is present in two or more of the microchannel structures of the microfluidic device provided in step (i). To each microchannel structure a single binder candidate or a combination of different binder candidates may be introduced into each microchannel structure in step (ii).

A larger extent of complex formation in the reaction microcavity of a particular microchannel structure will suggest that the binder used in this microchannel structure will have a stronger tendency to form an affinity complex than a binder giving a lower extent of complex formation in another microchannel structure.

This presumes that other reaction variables are kept essentially constant.

For other variants the meaning of a larger or smaller amount of retained complex in the reaction microcavity will depend on the particular protocol used. For certain protocols a larger amount will suggest a more efficient binder compared to a binder resulting in a smaller amount. For other protocols the opposite will be true.

In both variant (a) and (b) the reaction conditions may or may not differ between the individual microchannel structures.

The preferred protocols are the same as for alternative F below.

Formed affinity complexes can be further characterized with respect to the characteristics of the binder in the complex, for instance structure, binding characteristics, biological function etc.

C. Determination of immobilization techniques and/or solid phase that are suitable for a given affinity pair.

In this case at least the immobilization technique for the affinity reactant bound to the solid phase and/or the solid phase as such differ between two or more microchannel structures. The difference may relate to: conditions for physical adsorption, covalent attachment including kind of covalent bridge, affinity reactants used for affinity immobilization, kind of solid phase etc.

The meaning of a larger or smaller amount of retained complex in the reaction microcavity will depend on the protocols used. For certain protocols a larger amount will suggest an immobilization technique and/or a solid phase favoring binding compared to a technique giving smaller amount. For other protocols the opposite will be true.

D. Determination of suitable reaction conditions related to the liquid.

In this case at least one reaction variable related to the liquid varies between two or more microchannel structures in the microfluidic device. Typical reaction variables are pH, temperature, ionic strength, amount of an inhibitor or a promotor of complex formation, hydrogen-bond breaking agents, detergents, and flow rate in the microchannel structures etc.

The meaning of a larger or smaller amount of retained complex will depend on the protocols used. For certain protocols a larger amount will suggest an immobilization technique favoring binding compared to a technique giving smaller amount. For other protocols the opposite will be true.

E. Determination of a ligand and/or a binder with respect to their suitability for dissociation of their affinity complex.

These protocols typically start from microchannel structures in which the complex between the ligand and the binder is predisposed or preformed in immobilized form in the reaction microcavity. The complex may contain an analytically detectable reactant. Upon dissociation of the complex the analytically detectable reactant is released from the complex and the remaining amount of complex can be measured directly in the reaction microcavity or indirectly as the amount of released reactant in a separate detection microcavity positioned downstream the reaction microcavity. Alternatively the affinity counterpart that forms the link to the solid phase comprise a label that change as a function of the release of the other counterpart.

Suitable reaction variables that may be varied are given under "Definitions" above.

F. Determination of qualitative aspects of complex formation.

The present invention applies to flow conditions during formation or dissociation of affinity complexes on a solid phase that is retained in a reaction microcavity. One can envisage that the distribution of the complex in the solid phase (reaction microcavity) along the flow direction will reflect affinity constants and rates for association and dissociation etc under the conditions used, and that this distribution will depend on various factors such as kind of binder and ligand and their concentrations, and substitution degree and availability on the solid phase, kind of solid phase, pH, ionic strength, flow rate etc.

One can therefore conceive that refined information of qualitative aspects of binding can be accomplished by measuring this distribution, e.g. as the local amount of complex as a function of position in the solid phase (reaction microcavity) along the flow direction.

The requirement on intra-channel variation in residence time is strict, e.g. the variation should be within mean residence time \pm 75 %, such as \pm 50 % or \pm 25% or \pm 10 % or \pm 5 %.

A simple case is that one starts with a library of compounds (= binders) in which the individual members are of similar size. The library is then tested according to the invention in a microfluidic device in which two or more of the microchannel structures have the ligand immobilized in the reaction microcavity. Since the compounds are of the same size, the diffusion will be essentially the same for the members of the library. The local amount of complex as a function of position in the flow direction of the solid phase will therefore reflect the affinity between the compound and the ligand that has formed the complex in a particular microchannel structure. A sharp zone, for instance, in the initial part of the solid phase (reaction microcavity) could suggest a stronger affinity than a broader more diffuse zone that is located more downstream.

The distribution of a complex in the solid phase (reaction microcavity) may also be used as a function test for an assay, e.g. of the type discussed for alternative A above.

This innovative alternative requires that the binding reaction between an immobilized ligand and a binder takes place in the reaction microcavity and that the complex formed is measured in step (iii). The immobilized ligand may be introduced prior to formation of the complex. The ligand and binder may be any of the affinity counterparts given above for library members provided the formed complex can be retained in sufficient amount in the reaction microcavity. Typically the immobilized ligand is present in an unlimited amount. To facilitate the measurement in step (iii) properly selected detectable reactants can be included in one or more of steps (i)-(iii), e.g. a) the immobilized ligand may have

a label that change its signal upon formation of the immobilized complex, b) the binder may have a label meaning that the complex formed in step (ii) will comprise the label, c) a soluble analytically detectable affinity counterpart to the binder is used in a sandwich protocol etc.

A potentially interesting variant includes that two labels that are interacting with each other when in close proximity are used. A typical example is scintillation proximity assays (SPA) in which the ligand is labeled with tritium and the solid phase comprises a scintillation substance. SPA has found wide-spread use for screening of drug candidates, affinity ligands etc with respect to interaction properties.

Other interesting variants include sandwich protocols and displacement protocols as described above for alternative A with the proviso that the binder in this variant of the invention replaces the analyte.

A soluble analytically detectable affinity counterpart to the binder is preferably used when the binder is large and able to bind two affinity counterparts simultaneously, typically in sandwich protocols. The other labeled reactants that are mentioned above have great advantages for small binders.

In the context of this aspect of the invention, it may be interesting to determine relative affinity of a complex, binder and/or ligand in relation to various members of a library as defined under "Definitions" above.

By adapting the flow rates to implement reactions that are not diffusion-limited the main feature studied will be the affinity constants. This in particular applies to affinity reactants that are large.

Variants meaning that the formed affinity complex as such is determined are also possible to use in this alternative (F).

Samples

The samples used in one run of the innovative method correspond to a collection (library) of samples. At least two of the members of the collection differ with respect to the reaction variable(s) to be characterized.

Samples that differ with respect to reaction variables that are defined by soluble molecular entities can be introduced into the inlet ports of the microchannel structures in step (ii) or in step (iii). In the case the reaction variables are defined by insoluble entities (solid phases, immobilization techniques etc), the library is preferably provided in step (ii) together with the microfluidic device.

Different protocols may require different kind of samples and vice versa.

For alternatives A and B above, the samples are typically derived from biological material such as whole blood, plasma, serum, buffy coat, blood cells, semen, cerebrospinal fluid, lymph, lachrymal fluid, ascites, tissue, supernatants from cell lysates, cell culturing etc that has been treated in various ways in order to give aliquot 1. Included are also biologically material that has been produced synthetically such as synthetically produced oligo- and polypeptides, oligo- and polynucleotides, compounds that potentially are mimicking biological molecules or interactions etc.

For the other alternatives the samples typically are more or less synthetic.

Depending on the particular protocol, alternative F may utilize any of the abovementioned kinds of samples.

Measuring and Characterization (step (iii) and step (iv))

The measurement in step (iii) comprises measuring a) the distribution of the affinity complex in the reaction microcavity (solid phase) along the flow direction,

or b) the total amount of the complex in the reaction microcavity. The latter includes that measurement is carried out only in a certain part of the reaction microcavity as long as this amount is representative for the total amount.

Alternative (a) in particular applies to alternative (F) above.

A number of various ways of measuring immune complexes immobilized to a solid phase by utilizing analytically detectable affinity reactants are known in the field. In principle most of them can be used in the present invention.

Typical examples are spectroscopic methods based on chemiluminescence, bioluminescence, fluorescence with particular emphasis of laser-induced fluorescence (LIF) etc. As indicated elsewhere in this specification these spectroscopic principles often utilize reactants that are labeled with the corresponding analytically detectable group (label). Other principles are based on signals emanating from the complex as such, for instance turbidometry.

As already discussed step (iii) may comprise substeps in which analytically detectable affinity reactants are introduced for facilitating the measurement.

The characterization step (step (iv)) means that the measured value in step (iii) is used to characterize an uncharacterized reaction variable in the samples. This is common practice in the field and needs no further comments. In some cases when the inventive method results in a binding capacity for an unknown entity characterization for identifying the entity may be included in the method aspect of the invention.

The best mode corresponds to the work presented in the experimental part.

A SEPARATE ASPECT OF THE INVENTION.

A separate aspect of the invention is a structural unit (substructure) for reducing inter-channel variations in flow. The unit is illustrated in figure 3. The unit

comprises (a) an inlet microconduit (302), (b) a microcavity (304) in which a reaction is to take place under controlled flow conditions, and (c) an outlet microconduit (305). This device is characterized in that there are means for creating a pressure drop in the microcavity (304) and/or in the outlet microconduit (305) downstream the microcavity (304) so that the inter-channel variation in residence time within the microfluidic device for the samples introduced via the inlet microconduits (302) becomes within the limits discussed above. Suitable flow rates through the microcavity are typically within the intervals given above. The means for creating the pressure drop are as outlined in the earlier part of this specification.

In a preferred variant of this inventive aspect there is also an additional microconduit (103 in figures 1a, 306) merging with the inlet microconduit as illustrated in figures 1a and b. This additional microconduit may have various functions (vent, inlet etc) and intersects with the inlet microconduit (302), typically in close proximity to its joint with the reaction microcavity (304).

As discussed for figures 1a and b, and 2 the microchannel structures comprising this preferred substructure can be present in a substrate having an axis of symmetry and arranged so that inlet microconduit (302) and the additional conduit (103 in figure 1a) are at a larger radial distance than the outlet conduit (305) and the reaction microcavity at an intermediary radial distance (304). The substrate may comprise a plurality of this kind of microchannel structures/substructure oriented radially outwards from the axis of symmetry (spinning axis) and arranged to define two or more annular zones (rings) around the spinning axis, or sectors of such a zone. According to this aspect the microchannel structures in the same annular zone has the substructure at the same radial distance while the substructures for other annular zones are at a different radial distance. Since it is known that the centrifugal force at an outer position is larger than at an inner position, outlet microconduit (105,305) in an outer annular zone shall be longer than in an inner annular zone if the

hydrodynamic cross-sectional area is kept constant and the same liquid flow is desired for all the microchannel structures of this kind on the substrate.

Thus by varying the design (hydrodynamic cross-sectional area and/or length) it is possible to place several microchannel structures comprising the described substructure at different radial distances while maintaining the same flow rate through the reaction microcavity. Inversely this concept makes it possible to construct microfluidic devices in which there are microchannel structures in which the flow rate through the reaction microcavity will differ in a well-defined manner.

This aspect of the invention is useful in the method aspect of the invention (method for the characterization of reaction variables). This aspect may also be useful for other microfluidic applications where a controlled liquid flow is beneficial, e.g. microtitration and chemical synthesis in the microformat and other situations where controlled mixing or controlled addition of reagents are needed.

The patent applications given below have been discussed in this specification. All of them are hereby incorporated by reference, in particular those WO applications that designate the US.

WO 9116966, 9615576, WO 9721090, WO 9800709, 9807019, WO 9958245, WO 0056808, WO 0146465, WO 0147637, WO 0154810, WO 0185602, US 60/315,471 and corresponding International Patent Application, U.S. S.N. 60/322,622 and the c.i.p. US application filed on January 31, 2002.

EXPERIMENTAL PART

Figures 1-2 shows the structure used in this experiment.

A complete myoglobin assay was performed in a disc of the same dimension as a compact disc (CD). In the disc used there were 24 similar structures (101,201)

in parallel and the structures were divided in 2 sets each containing 12 structures (only one set is shown in figure 2). A common distribution channel (119, 219) connected the 12 structures, through which buffer and reagents were distributed to the 12 reaction structures via either inlet port (209) or inlet port (210). Every structure had also its individual inlet unit (108,114) designed with a sample receiving structure (111), which has a volume definition function. The dimensions of the channel are indicated in figures 1a-b.

In order to achieve capillary action in the reaction structures the CD surface was treated with O₂-plasma , subsequently a plastic lid was laminated to the CD. According to a standard procedure all structures were incubated with PEG-PEI WO 0056808 (Gyros AB) and WO 0147637 (Gyros AB). The PEG-PEI molecules bind to the surface and establish a layer with low protein adsorption. After the PEG-PEI incubation the structures were thoroughly washed with water.

The immunoassay was performed in an automated system. The system (instrument prototype, Gyros AB, Uppsala, Sweden) was equipped with CD-spinner, holder for Microtiter plates (MTP) and a robotic arm with a holder for a capillary connected to a syringe pump and 8 slit pins. The capillary transferred all reagents and buffers from a MTP to either of the two inlet units (209,210) of the common distribution channel (119) in the disc. The slit pins transferred individual samples from a MTP to the individual sample inlet units (108) in the disc.

The instrument prototype is a fully automated robotic system controlled by application-specific software. Microplates containing samples or reagents are stored in a carousel within the system. A high precision robot transfers samples from microplates or containers into the microworld of the CD. CDs are moved to the spinning station for the addition of samples and reagents. An application-specific method within the software controls the spinning at precisely controlled speeds controls the movement of liquids through the microstructures as the application proceeds.

Polystyrene particles (15 µm, Dynal Particles AS, Norway) were selected for the solid phase. The beads was modified by passive adsorption of phenyl-dextran to create a hydrophilic surface and were subsequently covalently coupled with a monoclonal antimyoglobin 8E.11.1 (LabAs, Tartu,Estonia) using CDAP chemistry (Kohn & Wilchek, Biochem. Biophys Res. Comm. 107 (1982) 878-884).

After coupling with the antibody, a suspension of the particles was distributed in the common distribution channel (119) via inlet unit (109) and moved through the structure by centrifugal force. The centrifugal force combined with the vents (122) divide the suspension in the channel in equal portions each of which forms a bed of packed particles (column) in the reaction microcavity (104) against the dual depth in front of the outlet conduit (105). The approximate volume of the column was 10 nl. The columns were washed once with 0.01 M Phosphate-buffer, pH 7.5 containing 0.15 M NaCl via the common distribution channel (119). Every addition of solution delivers 200 nl liquid to the individual column. One addition of washing solution is 20 times the column volume, which ensures a very efficient washing

To demonstrate the myoglobin assay in the system a 6-point standard curve was created. The myoglobin samples (diluted in PBS, 1%BSA) with concentrations in the range of 0-1620ng/ml where distributed to the individual inlet units by slit pins. The sample volume 100nl was defined in the sample receiving structure (111) (during the first two step in the spin flow method). To reach favourable kinetic condition under the capturing step (for myoglobin to bind) the flow rate of the sample should not exceed 1nl/sec. The sample flow rate was controlled by the spin velocity (spin flow1). After sample capturing the columns were washed twice by addition of PBS, 0.01% Tween to the common distribution channel followed by a spin step. Detection antibodies in excess were applied next via the common distribution channel, these were monoclonal antimyoglobin 2F9.1 (LabAs,Tartu) and a similar slow flow rate (spin flow 2) was used. The detecting antibodies

were labelled with a fluorophor Alexa 633 (Molecular Probes, Eugene, USA). Excess of labelled antibody was washed away in 4 additions of PBS-T.

The completed assay was analysed in a laser induced fluorescence (LIF) detector. The detector moved radially along the column while the disc was rotating. The results are presented in **Figure 4**. Signal intensity was typically concentrated to the top of the column.

The design of the Laser Induced Fluorescence (LIF) module was constructed for quantitative measurement of fluorescence in the microfluidic device (disc of CD format) used in the experiments.

The disc was rotated by means of a motor on a rotatable shaft; the speed could be varied from 60 to 3000 rpm. By means of an encoder and a fixed home position on the CD the position of each structure of interest could be stored in a file.

A pick-up head was constructed. It consisted of a laser whose beam was reflected on a dichroic mirror and focused onto the structure of interest in the disc through a 5x objective. The epi-fluorescent light passed through the dichroic mirror and through a band-pass filter, optimised for the flourochrome at hand. It was focused onto a PMT by means of an aspheric lens.

By rotating the disc while measuring a signal across the structure a trace was obtained corresponding to the fluorescence in the structure. By moving the pick-up means of a motor in radial direction while rotating the disc a measurement of the total fluorescence in the structure was obtained.

The detector is described in U.S. S.N. 60/322,622, SE 0103118-6, SE 010446-9 and US application filed on January 31, 2002 ("Arrangement and method for measurement in spinning microfluidic devices").

An overview of the run method in the system is presented in Tab 2.

Table1. An overview of the run method performed in the system

Run method	Spin profile
Wash of CD structures	
Spin1	5700rpm 15s
Transfer of beads	
Spin2	4500rpm 10s, 5000rpm 10s
Wash of beads	
Spin3	5800rpm 15s, 6700rpm 5s
Transfer of samples	
Spin flow1	1200rpm 2s, 2200rpm 0.5s, from 1700-2500rpm in 90sec. 3000rpm 15s, 5500rpm 5s
Myoglobin wash 1	
Spin4	4500rpm 20s, 5700rpm 5s
Myoglobin wash 2	
Spin5	4500rpm 20s, 5700rpm 5s
Transfer of conjugate	
Spin flow 2	2500rpm 0.6s, 1500-2500rpm in 120sec. 3000rpm 15s, 5500rpm 5s
Conjugate wash1	
Spin6	4500rpm 20s, 5700rpm 5s
Conjugate wash2	
Spin7	4500rpm 20s, 5700rpm 5s
Conjugate wash3	
Spin8	4500rpm 20s, 5700rpm 5s
Conjugate wash4	
Spin9	4500rpm 20s, 5700rpm 5s
Detection	

Certain innovative aspects of the invention is defined in more detail in the appending claims. Although the present invention and its advantages have been described in detail, it should be understood that various changes, substitutions and alterations can be made herein without departing from the spirit and scope of the invention as defined by the appended claims. Moreover, the scope of the present application is not intended to be limited to the particular embodiments of

the process, machine, manufacture, composition of matter, means, methods and steps described in the specification. As one of ordinary skill in the art will readily appreciate from the disclosure of the present invention, processes, machines, manufacture, compositions of matter, means, methods, or steps, presently existing or later to be developed that perform substantially the same function or achieve substantially the same result as the corresponding embodiments described herein may be utilized according to the present invention. Accordingly, the appended claims are intended to include within their scope such processes, machines, manufacture, compositions of matter, means, methods, or steps.

C L A I M S

1. A microscale method for the characterization of at least one reaction variable that influences the formation or dissociation of an affinity complex comprising a ligand and a binder, which have affinity for each other, **characterized in** comprising the steps of:
 - (i) providing a microfluidic device comprising a plurality of microchannel structures that are under common flow control, each microchannel structure comprising a reaction microcavity;
 - (ii) performing essentially in parallel an experiment in each of two or more of the plurality of microchannel structures, the experiment in these two or more microchannel structures comprising either
 - a) formation of an immobilized form of the complex and retaining under flow conditions said form within the reaction microcavity, or
 - b) dissociating, preferably under flow conditions, the immobilized form of the complex which has been introduced prior to step (ii), said at least one reaction variable being different or uncharacterized for said two or more microchannel structures;
 - (iii) measuring the presentation of the complex in said reaction microcavity in each of said two or more microchannel structures; and
 - (iv) characterizing said at least one reaction variable based on the values for presentation obtained in step (iii).
2. The method of claim 1, **characterized in** that each of the microcavities of said two or more microchannel structures comprises a solid phase to which an affinity reactant which is capable of being incorporated into the affinity complex retained in step (ii) is attached.
3. The method of any of claims 1-2, **characterized in** that
 - (a) the microfluidic device comprises a substrate having an axis of symmetry,
 - (b) each microchannel structure is oriented relative the axis of symmetry with an inlet port at shorter radial distance than the reaction microcavity, and

- (c) the substrate is spun around its axis of symmetry to drive liquid within the microchannel structures.
4. The method of any of claims 1-2, **characterized** in that
- a) the microfluidic device comprises a substrate having an axis of symmetry,
 - (b) each microchannel structure is oriented radially relative the axis of symmetry with the reaction microcavity at a larger radial distance than a substructure delivering liquid to the reaction microcavity, and
 - (c) the substrate is spun around its axis of symmetry to drive liquid within the microchannel structures.
5. The method of any of claims 1-4, **characterized** in that each of the microchannel structures comprises a flow restriction downstream the reaction microcavity, which creates a pressure drop that restricts the flow through the reaction microcavity.
6. The method of any of claims 1-5, **characterized** in that step (iii) is performed by measuring
- (a) distribution of the complex in the reaction microcavity along the flow direction, or
 - (b) the total amount of the complex in the reaction microcavity.
7. The method of any of claim 1-6, **characterized** in that step (iii) comprises measuring the total amount of the complex in the reaction microcavity.
8. The method of any of claims 1-7, **characterized** in that each of said experiments comprises formation of an immobilized form of the complex within the reaction microcavity.
9. The method of any of claims 1-7, **characterized** in that said experiment comprises dissociating under flow conditions an immobilized form of the

complex which complex is included in the microfluidic device provided in step (i).

10. The method of any of claims 1-9, **characterized** in that said at least one reaction variables that varies between the microchannel structure is selected amongst group 1 or group 2 reaction variables..
11. The method of any of claims 1-10, **characterized** in that the formation of the complex that is retained in the reaction microcavity is part of a competitive/inhibition protocol or a non-competitive protocol.
12. The method of claim 11, **characterized** in that said at least one reaction variable is related to an affinity reactant.
13. The method of claim 12, **characterized** in that said at least one the reaction variable is related to the amount of said affinity reactant.
14. The method of claim 12, **characterized** in that said at least one reaction variable is related to affinity of an affinity reactant.
15. The method of any of claims 1-14, **characterized** in that step (iii) comprises determining the distribution of the complex along the flow direction in the reaction microcavity in each of said two or more microchannel structures
16. The metod of claim 15, **characterized** in that step (iv) comprises that the relative affinity for the ligand and binder as a function of the variation in said at least one reaction variable is characterized.

Fig 1a

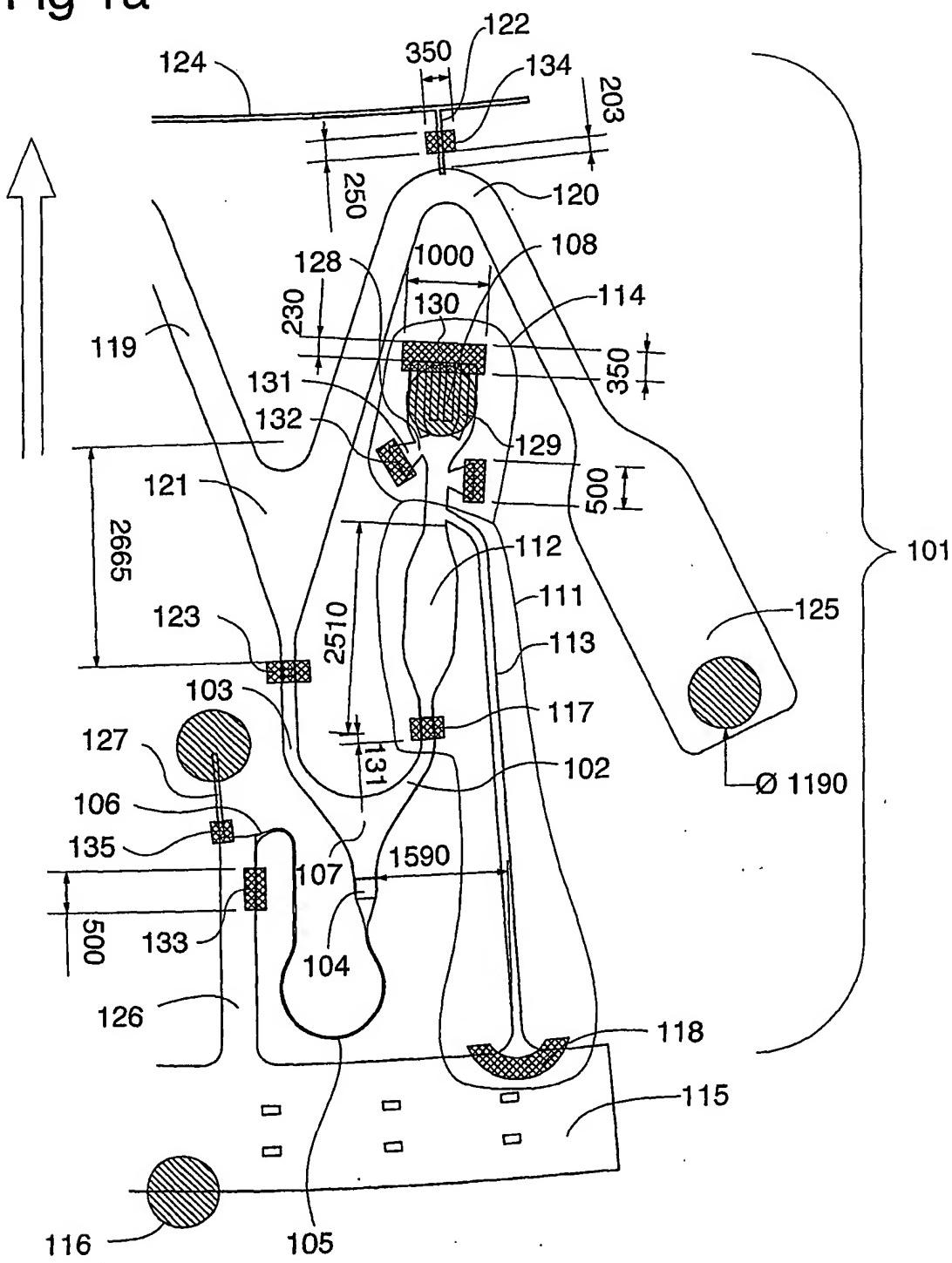
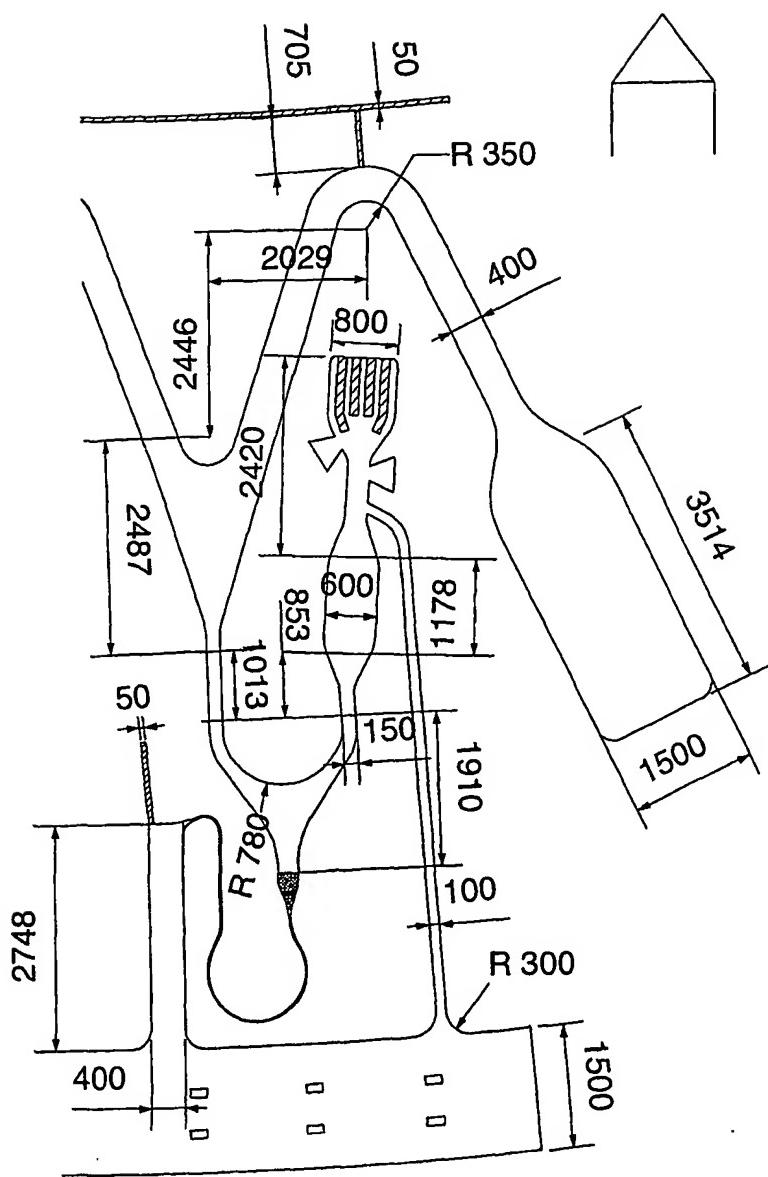


Fig 1b



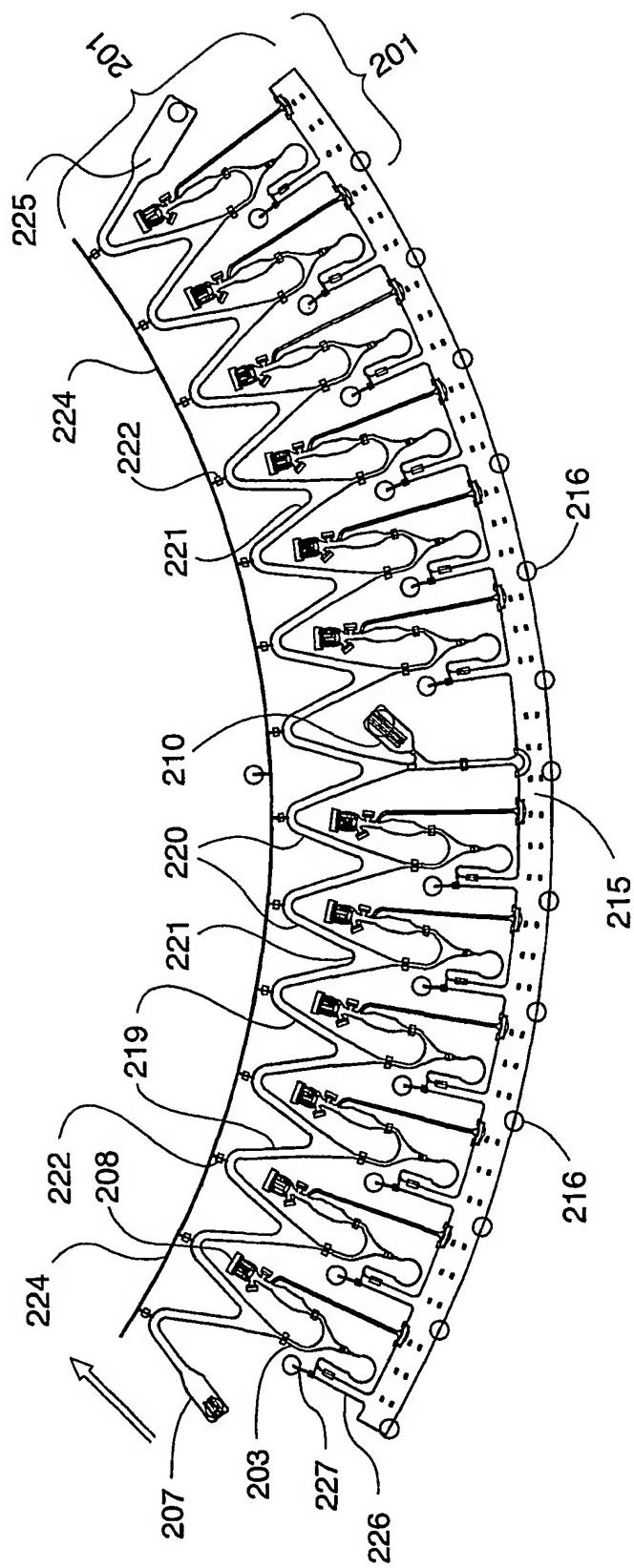
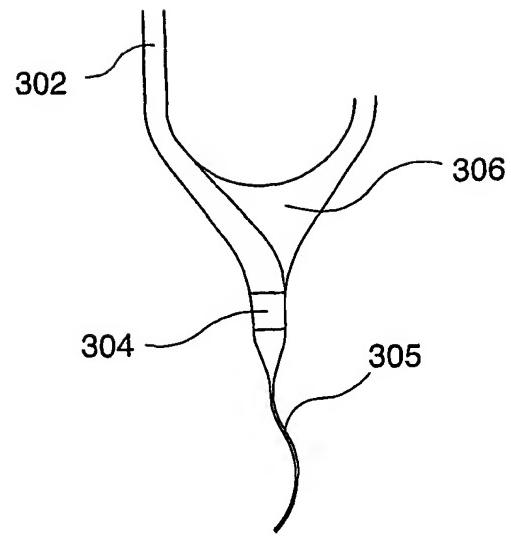


Fig 2

Fig. 3



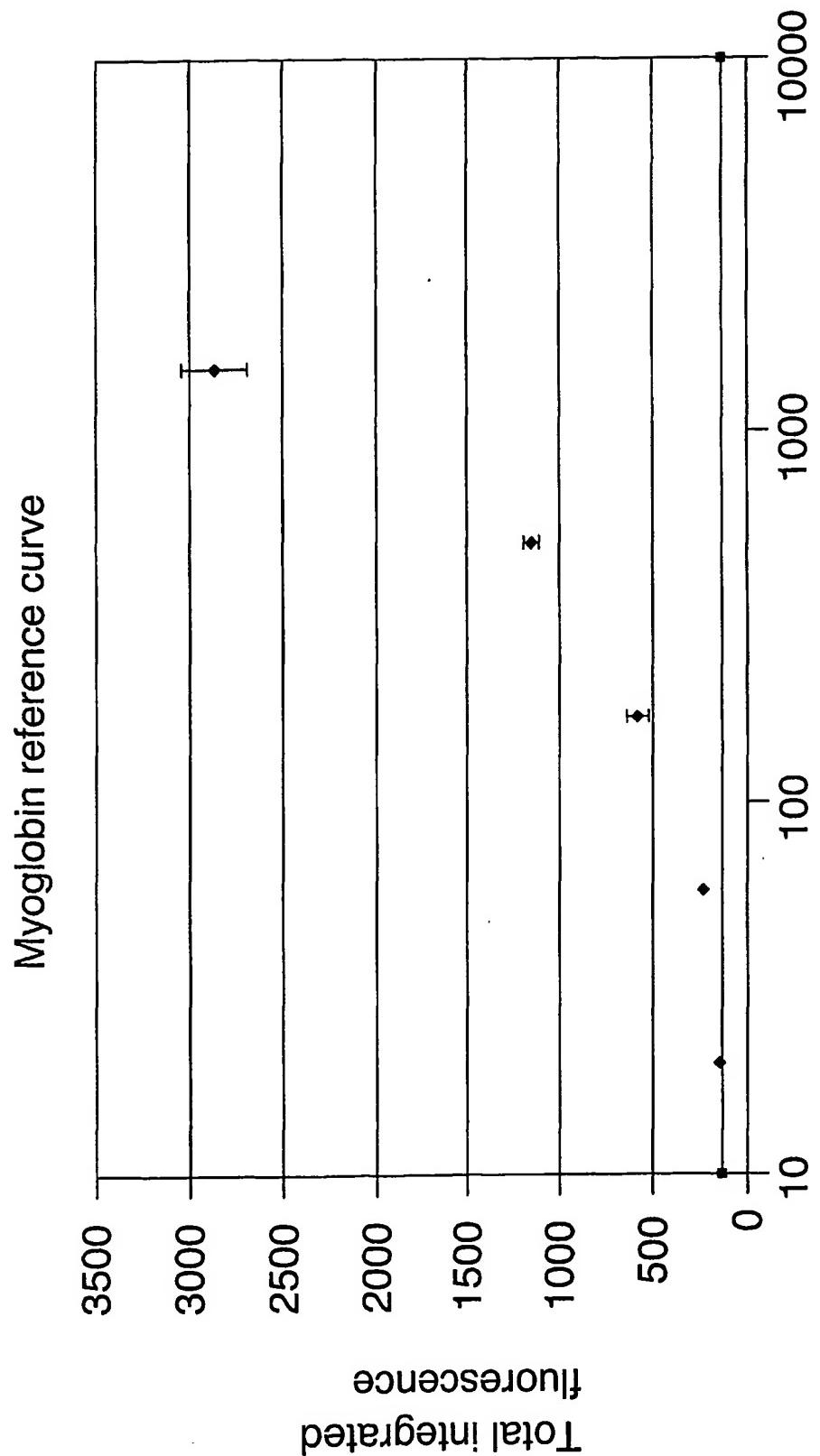


Fig 4 Concentration of myoglobin (ng/ml)

INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 02/00537

A. CLASSIFICATION OF SUBJECT MATTER

IPC7: G01N 33/543, B01L 3/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC7: B01L, G01N

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

WPI DATA

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 6143247 A (SHEPPARD, JR. ET AL), 7 November 2000 (07.11.00), abstract --	1-16
A	US 6046056 A (PARCE ET AL), 4 April 2000 (04.04.00), abstract --	1-16
A	WO 0062931 A1 (CLINICAL MICRO SENSORS, INC), 26 October 2000 (26.10.00), abstract -- -----	1-16

Further documents are listed in the continuation of Box C.

See patent family annex.

* Special categories of cited documents:

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INTERNATIONAL SEARCH REPORT
Information on patent family members

10/06/02

International application No. PCT/SE 02/00537	
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